

**COLLABORATORY FOR PROCESS
AND DYNAMIC SYSTEMS MODELING RESEARCH**

**COST MODULE FOR
GE RADIANT QUENCH IGCC ASPEN PLUS MODEL**

Report of

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to

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Introduction

This report describes the input parameters in the cost model developed for an integrated gasification combined cycle plant (IGCC) operating with a GE radiant quench gasifier. The performance model for this system was developed by the Department of Energy's National Energy Technology Laboratory (NETL) as an Aspen Plus steady-state process simulation. The performance model was delivered to Carnegie Mellon for the purpose of adding a cost model, as described in this report. Parameters from the performance model that are required for the cost model are identified in this report.

The cost model is divided into four separate areas: (1) financing parameters, (2) capital cost parameters, (3) operating and maintenance parameters, and (4) levelized cost parameters. Each input parameter is described briefly in the following sections. Intermediate and final result parameters are not described here; however, a final cost report is provided for two illustrative cases.

Aspen Plus Parameters

Power Generation or Use

The following power generation or electricity use parameters from the Aspen Plus flowsheet are used by the cost model. These parameters must be present in the Aspen Plus performance model.

| Parameter | Description | Units |
|-----------|--|-------|
| GTSUM | Gas turbine net power output | hp |
| STSUM | Power output from steam turbines | hp |
| WST | Power output from steam turbines (same as STSUM) | hp |
| WO2COM | Power for gasifier O ₂ compressor | hp |
| WASU | Power for air separation unit | hp |
| WN2COM | Power for N ₂ compressor | hp |
| WTGRPM | Power for tail gas pump | hp |
| WTGRCY | Power for tail gas recycle | hp |
| WCNDPM | Power for condensed water pump in steam cycle | hp |
| WGASEX | Power output from syngas expander | hp |
| WGT | Net power output of gas turbine system | hp |
| WHPPMP | Power of high pressure pump in steam cycle | hp |
| WIPPMP | Power of IP pump in steam cycle | hp |
| WLPPMP | Power of low pressure pump in steam cycle | hp |
| WQBOST | Power of quench water boost pump | hp |
| WQPMP | Power of quench water pump | hp |
| WSLRPM | Power of slurry preparation pump | hp |
| WSLYPM | Power of slurry pump | hp |
| WSYNBT | Power of booster for syngas from Selexol | hp |
| WTGREC | Power of tail gas recycle compressor | hp |
| WGTCOM | Power of gas turbine compressors | hp |

Temperatures and Pressures

The following temperature and pressure parameters from the Aspen Plus flowsheet are used by the cost model. These parameters must be present in the Aspen Plus performance model.

| Parameter | Description | Units |
|-----------|---|-------|
| PGASIF | Gasifier operation pressure | psi |
| TGASIF | Gasifier operation temperature | F |
| TFIRE | Operation temperature of gas turbine combustor | F |
| TCOMB | Temperature of gas mixture fed into gas turbine combustor | F |
| TGTOC | Temperature of exhaust from gas turbine | F |
| TSHSTM | Operation temperature of high pressure superheater in the steam cycle | F |
| TRESTM | Operating temperature of HRSG reheater | F |
| TLPSTM | Temperature of steam fed into the low pressure steam turbine | F |
| PHPS | Pressure of steam fed into the high pressure superheater | psi |

Flow Rates and Concentrations

The following flow rate and concentration parameters from the Aspen Plus flowsheet are used by the cost model. These parameters must be present in the Aspen Plus performance model.

| Parameter | Description | Units |
|-----------|---|----------|
| MCFGI | Mass flow of coal fed into the gasifier | lb/hr |
| PPEH2O | Moisture percentage in the coal | |
| O2IN | O ₂ mass flow from air separation unit | lb/hr |
| H2OIN | H ₂ O mass flow for coal slurry preparation | lb/hr |
| GTFUL1 | Syngas mass flow rate fed into gas turbine combustor | lb/hr |
| GTFUL2 | Syngas mass flow rate fed into gas turbine combustor | lb/hr |
| GTAIR | Air mass flow rate fed into gas turbine compressor | lb/hr |
| STSTM | Flow rate of main steam fed into high pressure steam turbine | lb/hr |
| FIPSTM | Mass flow rate of water fed into IP evaporator | lb/hr |
| FLPSTM | Mass flow rate of steam fed into the low pressure steam turbine | lb/hr |
| CO | Mole flow of CO fed into sour gas treatment unit (Selexol) | lbmol/hr |
| CO2 | Mole flow of CO ₂ fed into sour gas treatment unit (Selexol) | lbmol/hr |
| O2 | Mole flow rate of oxygen fed into gasifier | lbmol/hr |
| SGLT | Mass flow rate of syngas from quench unit | lb/hr |
| SGTOSR | Mole flow of syngas fed into Selexol unit for sulfur removal | lbmol/hr |
| SFRCL | Mass flow of sulfur from Claus unit | lb/hr |
| RH2O | Mass flow rate of make-up water in steam cycle | lb/hr |
| PH2O | Mass flow rate of water from condenser in steam cycle | lb/hr |
| HPS | Mass flow rate of steam fed into the high pressure superheater | lb/hr |
| SGTOSC | Mole flow rate of syngas from quench unit | lbmol/hr |

Input Parameters

Performance

Many of the cost parameters are linked directly to performance parameters already present in the Aspen Plus simulation delivered by NETL, as described in the previous section. However, several additional performance parameters must be added to satisfy the requirements of the cost model added to the simulation. These are described briefly below.

| Parameter | Description | Default Value | Units |
|--------------|--|---------------------|--------------|
| CF | Capacity Factor | 0.75 | Fraction |
| HHVCOAL | Coal Heating Value (HHV) | 11,666 | Btu/lb (wet) |
| NUMBER_LABOR | Total number of laborers | 20 | Laborers/day |
| YEAR | Construction Time ¹ | 4 | Years |
| NASU | Total ASU Operating Trains | 1 | Integer |
| T | Atmospheric Temperature | 59.0 | F |
| EFFASU | ASU Oxygen Purity | 0.95 | Fraction |
| NG | Total Gasifier Trains | 2 or 3 ² | Integer |
| NGO | Operating Gasifier Trains | 2 | Integer |
| NLT | Total Low Temp. Cooling Trains | 1 | Integer |
| NS | Total Selexol Sulfur Capture Trains | 1 | Integer |
| EFFS | Selexol Sulfur H ₂ S Removal Efficiency | 0.98 ³ | Fraction |
| NC | Total Claus System Trains | 2 | Integer |
| NBS | Total Beavon-Stretford System Trains | 2 | Integer |
| NGT | Total GE 7FB Gas Turbine Trains | 2 | Integer |
| NHR | Total Heat Recovery Steam Generator Trains | 1 | Integer |
| NST | Total Steam Turbine Trains | 1 | Integer |

¹ This is the idealized construction period in years. It is used to determine the allowance for funds used during construction (AFUDC).

² The number of total gasifier trains depends on whether a spare train is available or not.

³ This is the default value provided by the NETL Aspen Plus flowsheet.

Financing

This section describes the factors required to determine the carrying charge for all capital investments. The carrying charge is defined as the revenue required for the capital investment. The total charge can also be expressed as a levelized cost factor or fixed charge factor. The fixed charge factor is a function of many items. The fixed charge factor can be specified directly or calculated from the other input quantities below it on the financial input screen.

| Parameter | Description | Default Value | Units |
|-----------|---|---------------|------------------------|
| FCF | Fixed Charge Factor ⁴ | 0.14 | Fraction |
| DISCOUNT | Discount Rate (before taxes) ⁵ | 0.103 | Fraction |
| INFLATION | Inflation Rate ⁶ | 0.0 | Fraction |
| CPI | Chem. Eng. Cost Index Ratio ⁷ | 1.186 | Ratio of \$2005/\$2000 |

Capital Cost

The necessary capital cost input parameters associated with each process area in the IGCC flowsheet are listed below. The capital cost parameters and terminology used in the cost model are based on the methodologies developed by the Electric Power Research Institute (EPRI). EPRI has prepared a Technical Assessment Guide (TAG) in order to provide a consistent basis for reporting cost and revenues associated with the electric power industry (EPRI, 1986).

Total capital cost is divided into several specific cost areas, each of which is described in following sections:

- Process Facilities Cost
- General Facilities Cost
- Engineering & Home Office Fees
- Project Contingencies
- Process Contingencies
- Allowance for Funds Used During Construction (AFUDC)
- Royalty Fees
- Startup Costs
- Inventory Costs

These are summed and determine the total capital required. These can be annualized over the booklife of the power plant to give a levelized yearly cost. This levelized cost is used to determine the cost of electricity described in later sections.

⁴ The fixed charge factor is one of the most important parameters in financing. It determines the revenue required to finance the power plant based on the capital expenditures. Put another way, it is a levelized factor which accounts for the revenue per dollar of total plant cost that must be collected from customers in order to pay the carrying charges on that capital investment.

⁵ This is also known as the cost of money. Discount rate (before taxes) is equal to the sum of return on debt plus return on equity, and is the time value of money used in before-tax present worth arithmetic (i.e., levelization).

⁶ This is the rise in price levels caused by an increase in the available currency and credit without a proportionate increase in available goods or services. It does not include real escalation.

⁷ The cost information used was gathered in the year 2000. In order to report costs for the year 2006, a cost index is used (Vatavuk,1995).

Process Facility Cost (PFC)

The process facility cost (PFC) is composed of two parts: the direct construction costs and the indirect construction costs. The direct construction costs are provided in the cost model in equation form. The indirect construction costs are provided as a cost factor (shown below). The cost model provides an equation for each process area as a function of one or more performance parameters provided in the Aspen performance model.

| Parameter | Description | Default Value | Units |
|------------|---|---------------|-----------------|
| PFC_ASU | Air Separation Unit (ASU) Factor | 0.2 | Fraction of PFC |
| PFC_CH | Coal Handling System (CH) Factor | 0.2 | Fraction of PFC |
| PFC_G | Gasifier System (G) Factor | 0.2 | Fraction of PFC |
| PFC_LT | Low Temp. Gas Cooling System (LT) Factor | 0.2 | Fraction of PFC |
| PFC_PC | Process Condensate Treatment System (PC) Factor | 0.2 | Fraction of PFC |
| PFC_S | Selexol for Sulfur Removal System (S) ⁸ Factor | 0.2 | Fraction of PFC |
| PFC_C | Claus Plant (C) Factor | 0.2 | Fraction of PFC |
| PFC_BS | Beavon-Stretford Plant (BS) Factor | 0.2 | Fraction of PFC |
| PFC_BFW | Boiler Feedwater System (BFW) System | 0.2 | Fraction of PFC |
| PFC_GT | Gas Turbine System (GT) Factor | 0.2 | Fraction of PFC |
| PFC_HR | Heat Recovery Steam Generator System (HR) Factor | 0.2 | Fraction of PFC |
| PFC_ST | Steam Turbine System (ST) Factor | 0.2 | Fraction of PFC |
| PFC_N2COMP | Nitrogen Compressor (N2COMP) Factor | 0.2 | Fraction of PFC |

General Facility Cost

The general facilities include construction costs of roads, office buildings, shops, laboratories, etc. Sales taxes and freight costs are included implicitly. The cost typically ranges from 5-20% of the plant facility cost.

| Parameter | Description | Default Value | Units |
|------------|-------------------------------------|---------------|-----------------|
| GFC_ASU | ASU Factor | 0.15 | Fraction of PFC |
| GFC_CH | Coal Handling Factor | 0.15 | Fraction of PFC |
| GFC_G | Gasifier Factor | 0.15 | Fraction of PFC |
| GFC_LT | Low Temp. Gas Cooling Factor | 0.15 | Fraction of PFC |
| GFC_PC | Process Condensate Treatment Factor | 0.15 | Fraction of PFC |
| GFC_S | Selexol for Sulfur Factor | 0.15 | Fraction of PFC |
| GFC_C | Claus Plant Factor | 0.15 | Fraction of PFC |
| GFC_BS | Beavon-Stretford Factor | 0.15 | Fraction of PFC |
| GFC_BFW | Boiler Feedwater Factor | 0.15 | Fraction of PFC |
| GFC_GT | Gas Turbine Factor | 0.15 | Fraction of PFC |
| GFC_HR | Heat Recover Steam Generator Factor | 0.15 | Fraction of PFC |
| GFC_ST | Steam Turbine Factor | 0.15 | Fraction of PFC |
| GFC_N2COMP | Nitrogen Compressor Factor | 0.15 | Fraction of PFC |

⁸ A hydrolysis unit is assumed to be installed ahead of the selexol sulfur capture train. The capital cost of this hydrolysis unit is assumed to be 5% of the selexol sulfur capital cost.

Engineering & Home Office Fees

The engineering & home office fees are a percent of process facilities cost. This is an overhead fee paid to the architect/engineering company. These fees typically range from 7-15%.

| Parameter | Description | Default Value | Units |
|------------|-------------------------------------|---------------|-----------------|
| EHO_ASU | ASU Factor | 0.10 | Fraction of PFC |
| EHO_CH | Coal Handling Factor | 0.10 | Fraction of PFC |
| EHO_G | Gasifier Factor | 0.10 | Fraction of PFC |
| EHO_LT | Low Temp. Gas Cooling Factor | 0.10 | Fraction of PFC |
| EHO_PC | Process Condensate Treatment Factor | 0.10 | Fraction of PFC |
| EHO_S | Selexol for Sulfur Factor | 0.10 | Fraction of PFC |
| EHO_C | Claus Plant Factor | 0.10 | Fraction of PFC |
| EHO_BS | Beavon-Stretford Factor | 0.10 | Fraction of PFC |
| EHO_BFW | Boiler Feedwater Factor | 0.10 | Fraction of PFC |
| EHO_GT | Gas Turbine Factor | 0.10 | Fraction of PFC |
| EHO_HR | Heat Recover Steam Generator Factor | 0.10 | Fraction of PFC |
| EHO_ST | Steam Turbine Factor | 0.10 | Fraction of PFC |
| EHO_N2COMP | Nitrogen Compressor Factor | 0.10 | Fraction of PFC |

Project Contingency

This is a factor covering the cost of additional equipment or other costs resulting from a more detailed design. Higher contingency factors will be applied to simplified or preliminary designs and lower factors to detailed or finalized designs.

| Parameter | Description | Default Value | Units |
|-------------|-------------------------------------|---------------|-----------------|
| PROJ_ASU | ASU Factor | 0.15 | Fraction of PFC |
| PROJ_CH | Coal Handling Factor | 0.15 | Fraction of PFC |
| PROJ_G | Gasifier Factor | 0.15 | Fraction of PFC |
| PROJ_LT | Low Temp. Gas Cooling Factor | 0.15 | Fraction of PFC |
| PROJ_PC | Process Condensate Treatment Factor | 0.15 | Fraction of PFC |
| PROJ_S | Selexol for Sulfur Factor | 0.15 | Fraction of PFC |
| PROJ_C | Claus Plant Factor | 0.15 | Fraction of PFC |
| PROJ_BS | Beavon-Stretford Factor | 0.15 | Fraction of PFC |
| PROJ_BFW | Boiler Feedwater Factor | 0.15 | Fraction of PFC |
| PROJ_GT | Gas Turbine Factor | 0.15 | Fraction of PFC |
| PROJ_HR | Heat Recover Steam Generator Factor | 0.15 | Fraction of PFC |
| PROJ_ST | Steam Turbine Factor | 0.15 | Fraction of PFC |
| PROJ_N2COMP | Nitrogen Compressor Factor | 0.15 | Fraction of PFC |

Process Contingency

This quantifies the design uncertainty and cost of a commercial-scale system. This is generally applied on an area-by-area basis. Higher contingency factors are applied to new regeneration systems tested at a pilot plant and lower factors to full-size or commercial systems.

| Parameter | Description | Default Value | Units |
|-------------|-------------------------------------|---------------|-----------------|
| PROC_ASU | ASU Factor | 0.05 | Fraction of PFC |
| PROC_CH | Coal Handling Factor | 0.05 | Fraction of PFC |
| PROC_G | Gasifier Factor | 0.15 | Fraction of PFC |
| PROC_LT | Low Temp. Gas Cooling Factor | 0.00 | Fraction of PFC |
| PROC_PC | Process Condensate Treatment Factor | 0.10 | Fraction of PFC |
| PROC_S | Selexol for Sulfur Factor | 0.10 | Fraction of PFC |
| PROC_C | Claus Plant Factor | 0.10 | Fraction of PFC |
| PROC_BS | Beavon-Stretford Factor | 0.10 | Fraction of PFC |
| PROC_BFW | Boiler Feedwater Factor | 0.00 | Fraction of PFC |
| PROC_GT | Gas Turbine Factor | 0.125 | Fraction of PFC |
| PROC_HR | Heat Recover Steam Generator Factor | 0.025 | Fraction of PFC |
| PROC_ST | Steam Turbine Factor | 0.025 | Fraction of PFC |
| PROC_N2COMP | Nitrogen Compressor Factor | 0.05 | Fraction of PFC |

Royalty Fees

Royalty charges may apply to some portions of generating units incorporating new proprietary technologies.

| Parameter | Description | Default Value | Units |
|--------------|-------------------------------------|---------------|-----------------|
| ROYAL_ASU | ASU Factor | 0.005 | Fraction of PFC |
| ROYAL_CH | Coal Handling Factor | 0.005 | Fraction of PFC |
| ROYAL_G | Gasifier Factor | 0.005 | Fraction of PFC |
| ROYAL_LT | Low Temp. Gas Cooling Factor | 0.005 | Fraction of PFC |
| ROYAL_PC | Process Condensate Treatment Factor | 0.005 | Fraction of PFC |
| ROYAL_S | Selexol for Sulfur Factor | 0.005 | Fraction of PFC |
| ROYAL_C | Claus Plant Factor | 0.005 | Fraction of PFC |
| ROYAL_BS | Beavon-Stretford Factor | 0.005 | Fraction of PFC |
| ROYAL_BFW | Boiler Feedwater Factor | 0.005 | Fraction of PFC |
| ROYAL_GT | Gas Turbine Factor | 0.005 | Fraction of PFC |
| ROYAL_HR | Heat Recover Steam Generator Factor | 0.005 | Fraction of PFC |
| ROYAL_ST | Steam Turbine Factor | 0.005 | Fraction of PFC |
| ROYAL_N2COMP | Nitrogen Compressor Factor | 0.005 | Fraction of PFC |

Preproduction Startup Cost

These costs consider the operator training, equipment checkout, major changes in unit equipment, extra maintenance, and inefficient use of fuel or other materials during start-up. These are typically based on a portion of the total plant investment (TPI). The total plant investment is defined as:

$$\text{Total Plant Investment (TPI)} = \text{Plant Facility Cost} + \text{General Facility Cost} + \text{Engineering \& Home Office Fees} \\ + \text{Project Contingency} + \text{Process Contingency} + \text{AFUDC}$$

| Parameter | Description | Default Value | Units |
|----------------|-------------------------------------|---------------|-----------------|
| STARTUP_ASU | ASU Factor | 0.02 | Fraction of TPI |
| STARTUP_CH | Coal Handling Factor | 0.02 | Fraction of TPI |
| STARTUP_G | Gasifier Factor | 0.02 | Fraction of TPI |
| STARTUP_LT | Low Temp. Gas Cooling Factor | 0.02 | Fraction of TPI |
| STARTUP_PC | Process Condensate Treatment Factor | 0.02 | Fraction of TPI |
| STARTUP_S | Selexol for Sulfur Factor | 0.02 | Fraction of TPI |
| STARTUP_C | Claus Plant Factor | 0.02 | Fraction of TPI |
| STARTUP_BS | Beavon-Stretford Factor | 0.02 | Fraction of TPI |
| STARTUP_BFW | Boiler Feedwater Factor | 0.02 | Fraction of TPI |
| STARTUP_GT | Gas Turbine Factor | 0.02 | Fraction of TPI |
| STARTUP_HR | Heat Recover Steam Generator Factor | 0.02 | Fraction of TPI |
| STARTUP_ST | Steam Turbine Factor | 0.02 | Fraction of TPI |
| STARTUP_N2COMP | Nitrogen Compressor Factor | 0.02 | Fraction of TPI |

Operating & Maintenance Costs

Miscellaneous Unit Costs

Several unit costs are needed to determine key operating and maintenance costs. These are described briefly below.

| Parameter | Description | Default Value | Units |
|------------|---------------------------|---------------|---------|
| COAL_PRICE | Coal Price (As-delivered) | 1.34 | \$/MBtu |
| SUL_PRICE | Sulfur Credit Price | 58.0 | \$/ton |
| RATE_LABOR | Labor Rate | 24.82 | \$/hour |
| ASH_DIS | Ash Disposal Charge | 10.0 | \$/ton |

Maintenance Cost

The annual maintenance costs as given as a fraction of the process facilities capital cost. Maintenance cost estimates can be developed separately for different sections of the plant. Here are the default values for each section of the IGCC plant:

| Parameter | Description | Default Value | Units |
|------------|-------------------------------------|---------------|-----------------|
| MNT_ASU | ASU Factor | 0.02 | Fraction of PFC |
| MNT_CH | Coal Handling Factor | 0.02 | Fraction of PFC |
| MNT_G | Gasifier Factor | 0.035 | Fraction of PFC |
| MNT_LT | Low Temp. Gas Cooling Factor | 0.03 | Fraction of PFC |
| MNT_PC | Process Condensate Treatment Factor | 0.02 | Fraction of PFC |
| MNT_S | Selexol for Sulfur Factor | 0.02 | Fraction of PFC |
| MNT_C | Claus Plant Factor | 0.02 | Fraction of PFC |
| MNT_BS | Beavon-Stretford Factor | 0.02 | Fraction of PFC |
| MNT_BFW | Boiler Feedwater Factor | 0.015 | Fraction of PFC |
| MNT_GT | Gas Turbine Factor | 0.015 | Fraction of PFC |
| MNT_HR | Heat Recover Steam Generator Factor | 0.015 | Fraction of PFC |
| MNT_ST | Steam Turbine Factor | 0.015 | Fraction of PFC |
| MNT_N2COMP | Nitrogen Compressor Factor | 0.02 | Fraction of PFC |

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Illustrative Results

IGCC: GE Radiant/Quench Gasifier (no CO₂ Capture)

The following results are generated for the cost model added to the IGCC Aspen model. The IGCC plant included a GE entrained-flow gasifier with a radiant quench syngas cooling system, followed by a Selexol system to remove sulfur and a power block to generate electricity. The source code can be found in the appendix.

No Spare Gasifier Train

```
*** GASIFIER CONDITIONS ***
WET COAL FLOW RATE: 0.489685E+06 LB/HR
OXYGEN FLOW RATE: 0.387191E+06 LB/HR
WATER FLOW RATE: 0.201162E+06 LB/HR
GASIFIER PRESSURE: 814.7 PSIA
GASIFIER TEMPERATURE: 2400.0 F
GASIFICATION EFFICIENCY (HHV): 0.778

*** MS7000 GAS TURBINE CONDITIONS ***
FUEL FLOW RATE: 0.108905E+07 LB/HR
AIR FLOW RATE: 0.706498E+07 LB/HR
FIRING TEMPERATURE: 2538.0 F
COMBUSTOR EXIT TEMPERATURE: 663.5 F
TURBINE EXHAUST TEMPERATURE: 1121.1 F

*** STEAM TURBINE CONDITIONS ***
SUPERHEATED STEAM FLOW RATE: 0.157897E+07 LB/HR
SUPERHEATED STEAM TEMPERATURE: 1055.0 F
IP STEAM FLOW RATE: 0.152768E+06 LB/HR
REHEAT STEAM TEMPERATURE: 1055.0 F
LP STEAM FLOW RATE: 0.154450E+07 LB/HR
LP STEAM TEMPERATURE: 569.4 F

*** POWER PRODUCTION SUMMARY ***
GAS TURBINE: 0.463818E+09 WATTS
STEAM TURBINE: 0.300393E+09 WATTS
COMPRESSORS: -0.379552E+09 WATTS
OXYGEN PLANT: -0.578025E+08 WATTS
PLANT TOTAL: 0.646119E+09 WATTS
PLANT THERMAL EFFICIENCY (HHV): 0.386017E+00
```

COAL HEATING VALUE: 0.116660E+05 BTU/LB
CO2 EMISSION: 0.780930E+00 KG/KWH

*** ECONOMIC ASSUMPTION ***
CAPACITY FACTOR: 0.750
FIXED CHARGE FACTOR: 0.140
DISCOUNT RATE: 0.103
INFLATION RATE: 0.000
CONSTRUCTION YEAR: 4.000
COAL PRICE (\$/MMBTU): 1.340

*** IGCC CAPITAL COST SUMMARY (\$1000) ***

*** PROCESS FACILITY COST ***
AIR SEPARATION UNIT: 90573.1
COAL HANDLING: 75328.8
GASIFIER:142280.2
LOW TEMPERATURE GAS COOLING: 28161.5
PROCESS CONDENSATE: 17544.0
SELEXOL FOR SULFUR REMOVAL: 20212.6
CLAUS PLANT: 6709.4
BEAVON-STRETFORD UNIT: 0.0
BOILER FEED WATER: 1592.5
GAS TURBINE:112586.5
HRSG: 36511.3
STEAM TURBINE: 61990.3
N2 COMPRESSOR: 13571.9
TOTAL PROCESS FACILITY COST:607062.2

GENERAL FACILITY COST: 91059.3
ENGINEERING & OFFICE FEES: 60706.2
PROJECT CONTINGENCY: 91059.3
PROCESS CONTINGENCY: 50958.9
TOTAL PLANT COST: 900846.0
TOTAL PLANT COST (\$/KW): 1.3939
AFUDC:202166.9
TOTAL PLANT INVESTMENT: 1103012.9
ROYALTY: 3035.3
STARTUP: 29120.8
INVENTORY: 879.1
LAND: 2214.7
TOTAL CAPITAL REQUIREMENT: 1137383.7
TOTAL CAPITAL REQUIREMENT (\$/KW): 1.7599

ANNUAL VARIABLE O&M COST(\$/YEAR): 55498060.2635469
ANNUAL FIXED O&M COST(\$/YEAR): 29228278.8981885
COST OF ELECTRICITY(\$/MWH): 57.4699811930687

One Spare Gasifier Train

*** GASIFIER CONDITIONS ***
WET COAL FLOW RATE: 0.489685E+06 LB/HR
DRY COAL FLOW RATE: 0.686193E-39 LB/HR
OXYGEN FLOW RATE: 0.387191E+06 LB/HR
WATER FLOW RATE: 0.201162E+06 LB/HR
GASIFIER PRESSURE: 814.7 PSIA
GASIFIER TEMPERATURE: 2400.0 F
GASIFICATION EFFICIENCY (HHV): 0.778

*** MS7000 GAS TURBINE CONDITIONS ***

FUEL FLOW RATE: 0.108905E+07 LB/HR
 AIR FLOW RATE: 0.706498E+07 LB/HR
 FIRING TEMPERATURE: 2538.0 F
 COMBUSTOR EXIT TEMPERATURE: 663.5 F
 TURBINE EXHAUST TEMPERATURE: 1121.1 F

*** STEAM TURBINE CONDITIONS ***

SUPERHEATED STEAM FLOW RATE: 0.157897E+07 LB/HR
 SUPERHEATED STEAM TEMPERATURE: 1055.0 F
 IP STEAM FLOW RATE: 0.152768E+06LB/HR
 REHEAT STEAM TEMPERATURE: 1055.0 F
 LP STEAM FLOW RATE: 0.154450E+07LB/HR
 LP STEAM TEMPERATURE: 569.4 F

*** POWER PRODUCTION SUMMARY ***

GAS TURBINE: 0.463818E+09 WATTS
 STEAM TURBINE: 0.300393E+09 WATTS
 COMPRESSORS: -0.379552E+09 WATTS
 OXYGEN PLANT: -0.578025E+08 WATTS
 PLANT TOTAL: 0.646119E+09 WATTS
 PLANT THERMAL EFFICIENCY (HHV): 0.386017E+00
 COAL HEATING VALUE: 0.116660E+05 BTU/LB
 CO2 EMISSION: 0.780930E+00 KG/KWH

*** ECONOMIC ASSUMPTION ***

CAPACITY FACTOR: 0.750
 FIXED CHARGE FACTOR: 0.140
 DISCOUNT RATE: 0.103
 INFLATION RATE: 0.000
 CONSTRUCTION YEAR: 4.000
 COAL PRICE (\$/MMBTU): 1.340

*** IGCC CAPITAL COST SUMMARY (\$1000) ***

*** PROCESS FACILITY COST ***

AIR SEPARATION UNIT: 90573.1
 COAL HANDLING: 75328.8
 GASIFIER: 213420.4
 LOW TEMPERATURE GAS COOLING: 28161.5
 PROCESS CONDENSATE: 17544.0
 SELEXOL FOR SULFUR REMOVAL: 20212.6
 CLAUS PLANT: 6709.4
 BEAVON-STRETFORD UNIT: 0.0
 BOILER FEED WATER: 1592.5
 GAS TURBINE: 112586.5
 HRSG: 36511.3
 STEAM TURBINE: 61990.3
 N2 COMPRESSOR: 13571.9
 TOTAL PROCESS FACILITY COST: 678202.4

GENERAL FACILITY COST: 101730.4
 ENGINEERING & OFFICE FEES: 67820.2
 PROJECT CONTINGENCY: 101730.4
 PROCESS CONTINGENCY: 61629.9
 TOTAL PLANT COST: 1011113.2
 TOTAL PLANT COST (\$/KW): 1.5645

AFUDC:226912.9
TOTAL PLANT INVESTMENT: 1238026.1
ROYALTY: 3391.0
STARTUP: 32162.8
INVENTORY: 879.1
LAND: 2214.7
TOTAL CAPITAL REQUIREMENT: 1275794.7
TOTAL CAPITAL REQUIREMENT (\$/KW): 1.9740

ANNUAL VARIABLE O&M COST(\$/YEAR): 55498060.2635469
ANNUAL FIXED O&M COST(\$/YEAR): 33329746.6692580
COST OF ELECTRICITY(\$/MWH): 63.0009601724489

List of Abbreviations

| Abbreviation | Definition |
|-----------------|--|
| AFUDC | Allowance for Funds Used During Construction |
| ASU | Air Separation Unit |
| BTU | British Thermal Unit |
| CO ₂ | Carbon Dioxide |
| EPRI | Electric Power Research Institute |
| F | Fahrenheit |
| GE | General Electric |
| HHV | Higher Heating Value |
| HR | Hour |
| HRSG | Heat Recovery Steam Generation |
| IGCC | Integrated Gasification Combined Cycle |
| IP | Intermediate Pressure |
| kG | Kilogram |
| kW | Kilowatt |
| LB | Pound |
| LP | Low Pressure |
| MMBtu | 10 ⁶ Btu |
| MWh | Megawatt-Hours |
| N ₂ | Nitrogen |
| O ₂ | Oxygen |
| O&M | Operating and Maintenance |
| NETL | National Energy Technology Laboratory |
| PFC | Plant Facility Cost |
| PSIA | Pounds Per Square Inch Absolute |
| TAG | Technical Assessment Guide |
| TPI | Total Plant Investment |

Appendix

The Fortran source code used to define cost input parameters and calculate the cost results is listed below. This code has been embedded into the Aspen Plus flow sheet by means of a user block. In Aspen Plus, this code cannot be printed directly. However, a user can read and modify the code in the SUMMARY CALCULATOR found in in the flow sheet. To change any assumption in the cost model, find the parameters and change it.

```
C ----- REPORT GASIFIER CONDITIONS -----
C
F      MCOALD = MCFGI*(1.0-PERH2O/100.)
      HOC=11666.0
F      WRITE(*,110) MCFGI,MCOALD,O2IN,H2OIN,PGASIF,TGASIF
F 110  FORMAT(25X,'*** GASIFIER CONDITIONS ***',/
F      1  /11X,'      WET COAL FLOW RATE:',E14.6,' LB/HR',
F      2  /11X,'      DRY COAL FLOW RATE:',E14.6,' LB/HR',
F      3  /11X,'      OXYGEN FLOW RATE:',E14.6,' LB/HR',
F      4  /11X,'      WATER FLOW RATE:',E14.6,' LB/HR',
F      5  /11X,'      GASIFIER PRESSURE:',F8.1,' PSIA',
F      6  /11X,'      GASIFIER TEMPERATURE:',F8.1,' F'//)

C ----- REPORT GAS TURBINE CONDITIONS -----
F      WRITE(*,120) GTFULE,GTAIR,TFIRE,TCOMB,TGTPOC
F 120  FORMAT(/21X,'*** MS7000 GAS TURBINE CONDITIONS ***',/
F      1  /11X,'      FUEL FLOW RATE:',E14.6,' LB/HR',
F      2  /11X,'      AIR FLOW RATE:',E14.6,' LB/HR',
F      3  /11X,'      FIRING TEMPERATURE:',F8.1,' F',
F      4  /11X,'      COMBUSTOR EXIT TEMPERATURE:',F8.1,' F',
F      5  /11X,'      TURBINE EXHAUST TEMPERATURE:',F8.1,' F'//)

C ----- REPORT STEAM TURBINE CONDITIONS -----
F      WRITE(*,130) STSTM,TSHSTM,FIPSTM,TRESTM,FLPSTM, TLPSTM
F 130  FORMAT(/24X,'*** STEAM TURBINE CONDITIONS ***',/
F      1  /11X,'      SUPERHEATED STEAM FLOW RATE:',E14.6,' LB/HR',
F      2  /11X,'      SUPERHEATED STEAM TEMPERATURE:',F8.1,' F',
F      3  /11X,'      IP STEAM FLOW RATE:',E14.6,' LB/HR',
F      4  /11X,'      REHEAT STEAM TEMPERATURE:',F8.1,' F',
F      5  /11X,'      LP STEAM FLOW RATE:',E14.6,' LB/HR',
F      6  /11X,'      LP STEAM TEMPERATURE:',F8.1,' F'//)

C ----- REPORT POWER USAGE -----
      PWRNET=WST+W02COM+WASU+WN2COM+WTGRPM+WTGRCY+WCNDPM+WGASEX+WGT+
      & WHPPMP+WIPPMP+WLPMP+WQBOST+WQPMP+WSLRPM+WSLYPM+WSYNBT+WTGREC
      PWRNET=PWRNET+38162.30718+9364.3

F      PLANTEFF=-PWRNET*0.7455/(MCFGI*HOC*0.000293)
```

```

F      WRITE(*,140) -WGT*745.5*0.985, -WST*745.5, -WGTCOM*745.5,
      & -WASU*745.5, -PWRNET*745.5, PLANTEFF,HOC,
      & (CO+CO2)*44.04*0.4536/(-PWRNET*745.5/1000.0)
F 140 FORMAT(/23X,'*** POWER PRODUCTION SUMMARY ***'/
F 1 /11X,'          GAS TURBINE:',E16.6,' WATTS',
F 2 /11X,'          STEAM TURBINE:',E16.6,' WATTS',
F 3 /11X,'          COMPRESSORS:',E16.6,' WATTS',
F 4 /11X,'          OXYGEN PLANT:',E16.6,' WATTS',
F 5 /11X,'          PLANT TOTAL:',E16.6,' WATTS',
F 6 /11X,'PLANT THERMAL EFFICIENCY (HHV):',E16.6,
F 7 /11X,'          COAL HEATING VALUE:',E16.6,
F 8 /11X,'          CO2 EMISSION:',E16.6,' KG/KWH',/)

```

```

      COAL=MCFGI
C THERE IS NO B-S UNIT HERE, SO SET SULFUR FORM B-S IS 0
      SFRSB=0
      PGT=WGT
      PST=WST
      POWER=PWRNET

```

C THI BLOCK IS USED TO CALCULATE THE CAPITAL COST OF IGCC SYSTEM

C DIRECT COST OF THE MAJOR SECTIONS(\$1000 IN 2000)

C CAPACITY FACTOR

CF=0.75

C COAL HEATING VALUE (HHV,BTU/LB)

HHVCOAL=11666.0

C COAL_PRICE:\$/MMBTU

COAL_PRICE=1.34

C SULFUR PRICE (\$/TON)

SUL_PRICE=58.0

C LABOR NUMBER (WORKERS/DAY)

NUMBER_LABOR=20.0

C FIXED CHARGE FACTOR

FCF=0.14

C INFLATION RATE

INFLATION=0.0

C DISCOUNT RATE

DISCOUNT=0.103

C CONSTRUCTION PERIOD (YEAR)

YEAR=4.0

C OPERATION LABOR RATE (\$/HR)

RATE_LABOR=24.82

WRITE(*,145)CF,FCF,DISCOUNT,INFLATION,YEAR,COAL_PRICE

F 145 FORMAT(

F 1 /11X,' CAPACITY FACTOR:',F8.3,

F 2 /11X,' FIXED CHARGE FACTOR:',F8.3,

F 3 /11X,' DISCOUNT RATE:',F8.3,

F 4 /11X,' INFLATION RATE:',F8.3,

F 5 /11X,' CONSTRUCTION YEAR:',F8.3,

F 6 /11X,'COAL PRICE (\$/MMBTU):',F8.3/)

C Chemical Price Index based on US\$ in 2000

C Chemical Price Index - original costs are based on US\$ in 2000

C The cost is escalated to the current year prices (2005 US\$)

CPI=1.186

C ASU


```

NASU=1.0
T=59.0
EFFASU=0.95
DCASU=CPI*196.2*NASU*T**0.067/(1-EFFASU)**0.073*(O2/NASU)**0.5618
C COAL HANDLING
DCCH=CPI*9.92*COAL*0.454*24.0/1000.0
C GASIFIERS WITH ONE SPARING TRAIN (FROM FREY'S COST MODEL)
NG=2.0
NGO=2.0
DCG=CPI*1.1079*216*(COAL*0.4546/1000*24/NGO)**0.677*NG
C LOW TEMPERATURE GAS COOLING:
NLT=1.0
DCLT=CPI*0.0156*NLT*(SGLT/NLT)
C PROCESS CONDENSATE TREATMENT
SBD=380000.0*SGTOSC/56106.0
DCPC=CPI*9814*(SBD/300000.0)**0.6
C SELEXOL FOR SULFUR REMOVAL
NS=1.0
EFFS=0.98
DCS=CPI*0.304*NS/(1-EFFS)**0.059*(SGTOSR/NS)**0.98
C COS HYDROLYSIS DIRECT COST IS ESTIMATED AS 5% OF THAT OF SELEXOL FOR
C SULFUR REMOVAL, HENCE
DCS=1.05*DCS
C CLAUS UNIT
NC=2.0
DCC=CPI*6.96*NC*(SFRCL/NC)**0.668
C BEAVON-STRETFORD TAIL GAS REMOVAL
NBS=2
DCBS=(63.3+72.8*NBS*(SFRSB/NBS)**0.645)*0
C BOILER FEED WATER
TEMP=RH2O**0.307
TEMP2=PH2O**0.435
DCBFW=CPI*0.16*TEMP*TEMP2
C GAS TURBINE
NGT=2.0
DCGT=CPI*ABS(168.0*PGT/NGT*0.7455/1000.0)*NGT
C HRSG
NHR=1.0
DCHR=CPI*7.98/1000*NHR*PHPS**1.526*(HPS/NHR)**0.242
C STEAM TURBINE
NST=1.0
DCST=CPI*ABS(0.145*PST/NST*0.7455)
C N2 COMPRESSOR
DCN2COMP=CPI*13.0969*WN2COM**0.64
C PROCESS FACILITY COST FACTOR
PFCF_CH=0.2
PFCF_ASU=0.2
PFCF_G=0.2
PFCF_LT=0.2
PFCF_S=0.2
PFCF_C=0.2
PFCF_BS=0.2
PFCF_BFW=0.2
PFCF_PC=0.2
PFCF_GT=0.2
PFCF_HR=0.2
PFCF_ST=0.2
PFCF_N2COMP=0.2
C PROCESS FACILITY COST
PFC=(1+PFCF_CH)*DCCH+(1+PFCF_ASU)*DCASU+(1+PFCF_G)*DCG+

```

```

& (1+PFCF_LT)*DCLT+(1+PFCF_S)*DCS+(1+PFCF_C)*DCC+(1+PFCF_BS)*DCBS
& +(1+PFCF_BFW)*DCBFW
& +(1+PFCF_PC)*DCPC+(1+PFCF_GT)*DCGT+(1+PFCF_HR)*DCHR
& +(1+PFCF_ST)*DCST+(1+PFCF_N2COMP)*DCN2COMP

WRITE(*,150)(1+PFCF_ASU)*DCASU,(1+PFCF_CH)*DCCH,
& (1+PFCF_G)*DCG,(1+PFCF_LT)*DCLT,(1+PFCF_PC)*DCPC,
& (1+PFCF_S)*DCS,(1+PFCF_C)*DCC,(1+PFCF_BS)*DCBS,
& (1+PFCF_BFW)*DCBFW,(1+PFCF_GT)*DCGT,(1+PFCF_HR)*DCHR,
& (1+PFCF_ST)*DCST,(1+PFCF_N2COMP)*DCN2COMP,PFC
150 FORMAT(
F 2 /11X,' AIR SEPARATION UNIT:',F8.1
F 2 /11X,' COAL HANDLING :',F8.1,
F 3 /11X,' GASIFIER:',F8.1,
F 4 /11X,' LOW TEMPERATURE GAS COOLING:',F8.1,
F 4 /11X,' PROCESS CONDENSATE:',F8.1,
F 5 /11X,' SELEXOL FOR SULFUR REMOVAL:',F8.1,
F 6 /11X,' CLAU PLANT:',F8.1,
F 7 /11X,' BEAVON-STRETFORD UNIT:',F8.1,
F 8 /11X,' BOILER FEED WATER:',F8.1,
F 9 /11X,' GAS TURBINE:',F8.1,
F 9 /11X,' HRSG:',F8.1,
F 9 /11X,' STEAM TURBINE:',F8.1,
F 9 /11X,' N2 COMPRESSOR:',F8.1,
F 9 /11X,' TOTAL PROCESS FACILITY COST:',F8.1/)

C GENERAL FACILITY COST FACTOR
PFCF_GENERAL=0.15
C GENERAL FACILITY COST
PFC_GENERAL=PFCF_GENERAL*PFC
C ENGINEERING & HOME OFFICE FEE FACTOR
EHO_ASU=0.10
EHO_CH=0.10
EHO_G=0.10
EHO_LT=0.10
EHO_PC=0.10
EHO_S=0.10
EHO_C=0.10
EHO_BS=0.10
EHO_BFW=0.10
EHO_GT=0.10
EHO_HR=0.10
EHO_ST=0.10
EHO_N2COMP=0.10
C ENGINEERING & HOMW OFFICE FEES
ENGFEE=EHO_ASU*DCASU + EHO_CH*DCCH + EHO_G*DCG + EHO_LT*DCLT + EHO_PC*DCPC +
EHO_S*DCS + EHO_C*DCC + EHO_BS*DCBS + EHO_BFW*DCBFW + EHO_GT*DCGT + EHO_HR*DCHR +
EHO_ST*DCST + EHO_N2COMP*DCN2COMP
C PROJECT CONTINGENCY FACTORS
PROJ_ASU=0.15
PROJ_CH=0.15
PROJ_G=0.15
PROJ_LT=0.15
PROJ_S=0.15
PROJ_C=0.15
PROJ_BS=0.15
PROJ_BFW=0.15
PROJ_PC=0.15
PROJ_GT=0.15
PROJ_HR=0.15

```

PROJ_ST=0.15
PROJ_N2COMP=0.15

C PROJECT CONTINGENCY

PC_ASU=PROJ_ASU*(1+PFCF_ASU)*DCASU
PC_CH=PROJ_CH*(1+PFCF_CH)*DCCH
PC_G=PROJ_G*(1+PFCF_G)*DCG
PC_LT=PROJ_LT*(1+PFCF_LT)*DCLT
PC_S=PROJ_S*(1+PFCF_S)*DCS
PC_C=PROJ_C*(1+PFCF_C)*DCC
PC_BS=PROJ_BS*(1+PFCF_BS)*DCBS
PC_BFW=PROJ_BFW*(1+PFCF_BFW)*DCBFW
PC_PC=PROJ_PC*(1+PFCF_PC)*DCPC
PC_GT=PROJ_GT*(1+PFCF_GT)*DCGT
PC_HR=PROJ_HR*(1+PFCF_HR)*DCHR
PC_ST=PROJ_ST*(1+PFCF_ST)*DCST
PC_N2COMP=PROJ_N2COMP*(1+PFCF_N2COMP)*DCN2COMP

PROJECT_CONTINGENCY=PC_CH+PC_G+PC_LT+PC_S+PC_C+PC_BS+PC_BFW
& +PC_ASU+PC_PC+PC_GT+PC_HR+PC_ST+PC_N2COMP

C PROCESS CONTINGENCY FACTOR

PROC_CH=0.05
PROC_ASU=0.05
PROC_G=0.15
PROC_LT=0
PROC_S=0.1
PROC_C=0.1
PROC_BS=0.1
PROC_BFW=0
PROC_PC=0.1
PROC_GT=0.125
PROC_HR=0.025
PROC_ST=0.025
PROC_N2COMP=0.025

P_ASU=PROC_ASU*(1+PFCF_ASU)*DCASU
P_CH=PROC_CH*(1+PFCF_CH)*DCCH
P_G=PROC_G*(1+PFCF_G)*DCG
P_LT=PROC_LT*(1+PFCF_LT)*DCLT
P_S=PROC_S*(1+PFCF_S)*DCS
P_C=PROC_C*(1+PFCF_C)*DCC
P_BS=PROC_BS*(1+PFCF_BS)*DCBS
P_BFW=PROC_BFW*(1+PFCF_BFW)*DCBFW
P_PC=PROC_PC*(1+PFCF_PC)*DCPC
P_GT=PROC_GT*(1+PFCF_GT)*DCGT
P_HR=PROC_HR*(1+PFCF_HR)*DCHR
P_ST=PROC_ST*(1+PFCF_ST)*DCST
P_N2COMP=PROC_N2COMP*(1+PFCF_N2COMP)*DCN2COMP

PROCESS_CONTINGENCY=P_CH+P_G+P_LT+P_S+P_C+P_BS+P_BFW+P_PC+P_GT
& +P_ASU+P_HR+P_ST+P_N2COMP

C TOTAL PLANT COST

TPC=PFC+PFC_GENERAL+ENGFEE+PROJECT_CONTINGENCY
\$ +PROCESS_CONTINGENCY

C AFUDC

AFUDC=TPC*((1.0+DISCOUNT)**YEAR-(1.0+INFLATION)**YEAR)/

```

& (YEAR*LOG((1+DISCOUNT)/(1+INFLATION)))-1.0)
C TOTAL PLANT INVESTMENT
  TPI=TPC+AFUDC

C *****
C ANNUAL LABOR COST ($/YEAR)
  COST_LABOR=RATE_LABOR*NUMBER_LABOR*8760.0
C ANNUAL MANAGEMENT COST ($/YEAR)
  COST_MANAGE=0.65*COST_LABOR
C ANNUAL MAINTANCE COST ($/YEAR)

  MNT_ASU=0.02
  MNT_CH=0.02
  MNT_G=0.035
  MNT_LT=0.03
  MNT_PC=0.02
  MNT_S=0.02
  MNT_C=0.02
  MNT_BS=0.02
  MNT_BFW=0.015
  MNT_GT=0.015
  MNT_HR=0.015
  MNT_ST=0.015
  MNT_N2COMP=0.02
  COST_MAINTANCE = TPC/(PFC/1.2)*(MNT_ASU*DCASU + MNT_CH*DCCH + MNT_G*DCG +
MNT_LT*DCLT + MNT_PC*DCPC + MNT_S*DCS + MNT_C*DCC + MNT_BS*DCBS + MNT_BFW*DCBFW +
MNT_GT*DCGT + MNT_HR*DCHR + MNT_ST*DCST + MNT_N2COMP*DCN2COMP)*1000.0

C ANNUAL FIXED OPERATION COST ($/YEAR)
  FOC=COST_LABOR+COST_MANAGE+COST_MAINTANCE

C ANNUAL CONSUMABLES ($/YEAR)
  CONSUM=COAL/355940.0*3991712.0
C FUEL CONSUMABLES ($/YEAR):
  COAL_COST=COAL*HHVCOAL*8760*CF/1000.0/1000.0*COAL_PRICE
C ASH DISPOSAL COST ($/YEAR)
  ASH_DIS=10.0
  ASH_COST=22.65/355940.0*COAL*24.0*365.0*CF*ASH_DIS
C SULFUR BY PRODUCT CREDIT
  SUL_CREDIT=(SFRCL+SFRSB)/2000.0*8760.0*CF*SUL_PRICE

C ANNUAL VARIABLE OPERATION COST ($/YEAR)
  VOC=CONSUM+COAL_COST+ASH_COST-SUL_CREDIT
C *****

C TOTAL CAPITAL REQUIREMENT

  ROYAL_ASU=0.005
  ROYAL_CH=0.005
  ROYAL_G=0.005
  ROYAL_LT=0.005
  ROYAL_PC=0.005
  ROYAL_S=0.005
  ROYAL_C=0.005
  ROYAL_BS=0.005
  ROYAL_BFW=0.005
  ROYAL_GT=0.005
  ROYAL_HR=0.005
  ROYAL_ST=0.005
  ROYAL_N2COMP=0.005

```

ROYALTY=ROYAL_ASU*DCASU + ROYAL_CH*DCCH + ROYAL_G*DCG + ROYAL_LT*DCLT +
ROYAL_PC*DCPC + ROYAL_S*DCS + ROYAL_C*DCC + ROYAL_BS*DCBS + ROYAL_BFW*DCBFW +
ROYAL_GT*DCGT + ROYAL_HR*DCHR + ROYAL_ST*DCST + ROYAL_N2COMP*DCN2COMP

aINVENTORY=COAL/355940.0*639.0

C PREPRODUCTION STARTUP COSTS (only the capital portion - O&M omitted)

STARTUP_ASU=0.02
STARTUP_CH=0.02
STARTUP_G=0.02
STARTUP_LT=0.02
STARTUP_PC=0.02
STARTUP_S=0.02
STARTUP_C=0.02
STARTUP_BS=0.02
STARTUP_BFW=0.02
STARTUP_GT=0.02
STARTUP_HR=0.02
STARTUP_ST=0.02
STARTUP_N2COMP=0.02

STARTUP=TPI * (STARTUP_ASU + STARTUP_CH + STARTUP_G +
STARTUP_LT + STARTUP_PC + STARTUP_S + STARTUP_C + STARTUP_BS + STARTUP_BFW +
STARTUP_GT + STARTUP_HR + STARTUP_ST + STARTUP_N2COMP)

STARTUP=STRATUP+(VOC+FOC)/12/1000.
aLAND=ABS(POWER)*0.7455/1000/505.0*1731.0
TCR=TPI+ROYALTY+STARTUP+aINVENTORY+aLAND

F WRITE(*,160) PFC_GENERAL,ENGFEE,PROJECT_CONTINGENCY,
& PROCESS_CONTINGENCY,TPC,
& TPC/ABS(POWER*0.7457), AFUDC,TPI,ROYALTY,STARTUP,
& aINVENTORY,aLAND,TCR,TCR/ABS(POWER*0.7457)

F 160 FORMAT(
F 2 /11X,' GENERAL FACILITY COST:',F8.1
F 2 /11X,'ENGINEERING & OFFICE FEES:',F8.1
F 2 /11X,' PROJECT CONTINGENCY :',F8.1,
F 3 /11X,' PROCESS CONTINGENCY:',F8.1,
F 4 /11X,' TOTAL PLANT COST:',F10.1,
F 4 /11X,' TOTAL PLANT COST (\$/kW):',F8.4,
F 4 /11X,' AFUDC:',F8.1,
F 5 /11X,' TOTAL PLANT INVESTMENT:',F10.1,
F 6 /11X,' ROYALTY:',F8.1,
F 7 /11X,' STARTUP:',F8.1,
F 8 /11X,' INVENTORY:',F8.1,
F 9 /11X,' LAND:',F8.1,
F 9 /11X,'TOTAL CAPITAL REQUIREMENT:',F10.1,
F 9 /11X,' TCR/kw:',F8.4/)

VOC=CONSUM+COAL_COST+ASH_COST-SUL_CREDIT

C COE (\$/kWh)

COE=(1000.0*FCF*TCR+(FOC+VOC))/(ABS(POWER*0.7455)/1000.0)/
& (CF*8760.0)

WRITE(*,*) 'ANNUAL VARIABLE O&M COST(\$/YEAR):',VOC
WRITE(*,*) ' ANNUAL FIXED O&M COST(\$/YEAR):',FOC
WRITE(*,*) ' COST OF ELECTRICITY(\$/MWh):',COE